

# An ultra-short polarization beam splitter based on dual-core photonic crystal fiber with surface plasmon resonance effect

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**Abstract.** In this paper, an ultra-short polarization beam splitter (PBS) based on dual-core photonic crystal fiber (DC-PCF) with surface plasmon resonance (SPR) effect is proposed. The finite element method is used to investigate the coupling characteristics between the core mode and surface plasmon polariton (SPP) mode. The influences of the PCF structure parameters on the coupling length ( $CL$ ) and coupling length ratio ( $CLR$ ) are also investigated. The normalized output powers of the x-polarization and y-polarization are calculated, and the optimized PBS achieves an ultra-short length of 62.5  $\mu\text{m}$ . The splitting bandwidth of 110 nm (1.51~1.61  $\mu\text{m}$ ) is achieved when the extinction ratio ( $ER$ ) is less than -20 dB. The minimum  $ER$  reaches -71 dB at the wavelength of 1.55  $\mu\text{m}$ . The proposed PBS has an important application in the high-speed optical communication system.

**Keywords:** polarization beam splitter, photonic crystal fiber, surface plasmon resonance, extinction ratio.

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## 1. Introduction

With the rapid development of the communication system, the polarization characteristics of optics have attracted great attention. Because the polarization beam splitter (PBS) can split a beam of light into two polarized beams 1, it has widespread applications in optical communication and sensing systems. The larger refractive index difference between the two polarization beams is the key to achieve the PBS with shorter length and wider bandwidth. However, it is difficult to obtain the larger refractive index difference for the traditional dual-core optical fibers because of their structural symmetry and low birefringence 2. Compared with the traditional optical fibers, photonic crystal fiber (PCF) has unique optical characteristics, such as endlessly single-mode 5,6, high birefringence 7, large mode field area 10, controllable dispersion 11, and high nonlinearity 12. Thus, the PCF can be applied for different devices. For example, the PCF-based PBS with shorter length and wider bandwidth could be -achieved.

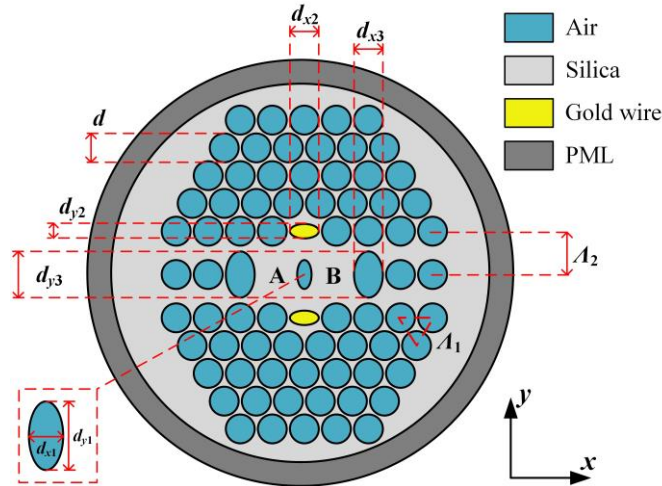
In recent years, some researchers designed different kinds of PBS based on the dual-core PCF (DC-PCF) through breaking the structural symmetry of the DC-PCF, which can be achieved by changing the arrangement of the air holes in the cladding region 19 or introducing the elliptical air holes 19. Moreover, other materials can also be used for replacing the silica substrate and the metal materials can be used for coating or filling the air holes. In 2015, Xu *et al.* reported a DC-PCF PBS with an elliptical hole, which is filled with a kind of low refractive index material. The length and bandwidth of the reported PBS are 401  $\mu\text{m}$  and 140 nm 22. In

43 2016, Wang *et al.* designed a DC-PCF PBS filled with the liquid crystal in the air hole, achieving  
 44 the PBS length of 890.5  $\mu\text{m}$  and bandwidth of 150 nm 23. In 2017, Wang *et al.* proposed a DC-  
 45 PCF PBS with the magnetic fluid added in the air hole, where the PBS length and bandwidth are  
 46 5.1 mm and 189 nm 24. In 2018, Wang *et al.* reported a rectangular-hexagonal structure DC-PCF  
 47 PBS with two elliptical holes in the core region, along with the PBS length of 93.3  $\mu\text{m}$  and  
 48 bandwidth of 40 nm 25. In 2019, Xu *et al.* demonstrated a DC-PCF PBS filled with titanium and  
 49 low refractive index liquid, where the PBS length and bandwidth are 83.9  $\mu\text{m}$  and 32.1 nm 26. In  
 50 2020, Qu *et al.* investigated a gold-coated silicon DC-PCF PBS, where the PBS length and mid-  
 51 infrared bandwidth are 192  $\mu\text{m}$  and 830 nm 27.

52 In this paper, we propose an ultra-short PBS based on the gold-filled DC-PCF. The two cores  
 53 of the DC-PCF are composed by the three elliptical air holes in the horizontal axis. Two elliptical  
 54 gold wires are filled in longitudinal axis to induce the surface plasmon resonance (SPR) effect.  
 55 The PBS can achieve an ultra-short length of 62.5  $\mu\text{m}$  and a bandwidth of 110 nm. The proposed  
 56 DC-PCF PBS has an important application in the high-speed optical communication system.

## 57 2. Design of the DC-PCF PBS and theory

58 The cross-section of the proposed DC-PCF PBS is shown in Fig. 1. The diameter of all circular  
 59 air holes arranged in the triangular array is  $d$ , and the hole-to-hole pitch is  $A_1$ . In addition, the  
 60 three layers of air holes are arranged in a rectangular array in the horizontal direction, and the  
 61 hole-to-hole pitch is  $A_2$ . The air hole in the most center is replaced with an elliptical hole, whose  
 62 minor and major axes are denoted by  $d_{x1}$  and  $d_{y1}$ , respectively. And the two air holes are missing  
 63 on the left and right sides of the central elliptical air hole to form the cores A and B, respectively.  
 64 The air holes on the upper and lower sides of the central elliptical hole are filled by the two  
 65 elliptical gold wires, whose minor and major axes are denoted by  $d_{y2}$  and  $d_{x2}$ , respectively.  
 66 Compared with other metal materials, the gold material has stable chemical property, good  
 67 biomolecular compatibility, and strong corrosion resistance. The left side of the core A and right  
 68 side of the core B are replaced by the two large elliptical air holes, whose minor and major axes  
 69 are denoted by  $d_{x3}$  and  $d_{y3}$ , respectively.



70  
71 **Fig. 1.** The cross-section of the proposed DC-PCF PBS.

72 The background material is the pure silica. The perfect matching layer (PML) of the  
 73 proposed DC-PCF is set at the outermost layer to absorb the radiation energy 28. The inner  
 74 diameter and thickness of the PML are 6  $\mu\text{m}$  and 1.2  $\mu\text{m}$ , respectively. The material of the PML

75 is highly doped silica, and the corresponding refractive index is  $n_{\text{silica}}+0.03$ . The material  
 76 dispersions of the silica and doped silica can be described by the Sellmeier equation [29, 30].  
 77 The dielectric constant of the gold material can be described by the Drude-Lorentz 31

$$\varepsilon_m = \varepsilon_\infty - \frac{\omega_D^2}{\omega(\omega + j\gamma_D)} - \frac{\Delta\varepsilon \cdot \Omega_L^2}{(\omega^2 - \Omega_L^2) - j\Gamma_L\omega}, \quad (1)$$

78 where  $\varepsilon_m$  represents the dielectric constant of gold,  $\varepsilon_\infty = 5.9673$  is the high frequency dielectric  
 79 constant,  $\Delta\varepsilon = 1.09$  is the wave vector,  $\omega$  is the angular frequency of the light, and  $\omega_D$  and  $\gamma_D$  are  
 80 the plasma frequency and Damping frequency, respectively. Here,  $\omega_D/2\pi = 2113.6$  THz, and  
 81  $\gamma_D/2\pi = 15.92$  THz.  $\Omega_L$  and  $\Gamma_L$  are the frequency and spectral width of the Lorentz oscillation,  
 82 respectively.  $\Omega_L/2\pi = 650.07$  THz, and  $\Gamma_L/2\pi = 104.86$  THz.

83 The coupling length ( $CL$ ) of the DC-PCF, where the light power is completely transferred  
 84 from one core to the other one, can be calculated by 32

$$CL_{x,y} = \frac{\lambda}{2(n_{x,y}^{\text{even}} - n_{x,y}^{\text{odd}})}, \quad (2)$$

85 where the  $CL_{x,y}$  is the  $CL$  of the  $x$ -pol and  $y$ -pol,  $\lambda$  is the wavelength of the incident light, and  $n$  is  
 86 the effective refractive indices of the even and odd modes. In order to achieve the complete beam  
 87 splitting, the  $CL$  of the two polarization states needs to satisfy the condition that  $mCL_x = nCL_y =$   
 88  $L$  ( $m$  and  $n$  are the positive integers and  $L$  is the length of the PBS), and the coupling length ratio  
 89 ( $CLR$ ) can be calculated by

$$CLR = \frac{CL_y}{CL_x}, \quad (3)$$

90 When the  $CLR$  reaches 2 or 0.5, the splitting length is the optimum value. The transmission  
 91 loss of the ultra-short PBS is also negligible. Therefore, when the input power  $P_{\text{in}}$  is determined,  
 92 the normalized output power  $P_{\text{out}}$  can be calculated by 33

$$P_{\text{out}}^{x,y} = P_{\text{in}}^{x,y} \cos^2\left(\frac{\pi L}{2CL_{x,y}}\right), \quad (4)$$

93 The performance of the PBS can be described by the extinction ratio ( $ER$ ) as following 34

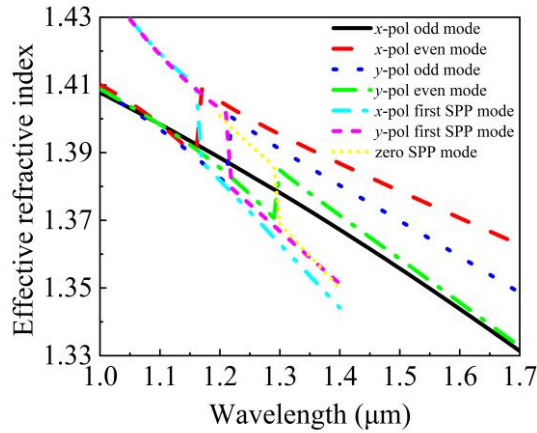
$$ER = 10 \cdot \lg\left(\frac{P_{\text{out}}^y}{P_{\text{out}}^x}\right), \quad (5)$$

94 when the  $ER$  is larger than 20 dB, the propagated light could be completely split, so the  $ER$   
 95 can determine the bandwidth of the PBS.

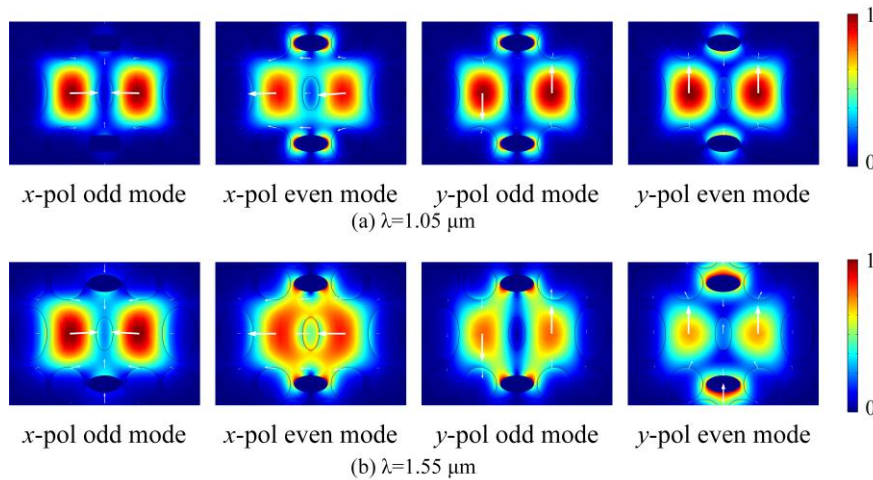
### 96 3. Simulation results and discussion

97 The finite element method (FEM) is adopted to simulate the proposed DC-PCF PBS. Fig. 2  
 98 shows the calculated effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and  
 99 even modes,  $x$ -pol and  $y$ -pol first SPP modes, and zero SPP mode. From Fig. 2, the  $x$ -pol even  
 100 mode and  $x$ -pol first SPP mode have a resonance point at wavelength 1.17  $\mu\text{m}$ , the  $y$ -pol odd  
 101 mode and  $y$ -pol first SPP mode have a resonance point at wavelength 1.22  $\mu\text{m}$ , and the  $y$ -pol

102 even mode and zero SPP mode have a resonance point at wavelength  $1.3 \mu\text{m}$ , while there is no  
 103 resonance point between the  $x$ -pol odd mode and SPP mode. According to the coupling mode  
 104 theory 35, the  $x$ -pol even,  $y$ -pol odd, and  $y$ -pol even modes are completely coupled with the  $x$ -pol  
 105 first SPP,  $y$ -pol first SPP, and zero SPP modes, respectively. In order to further verify the above  
 106 conclusions, the mode field distributions of the  $x$ -pol and  $y$ -pol even and odd modes at  
 107 wavelengths  $1.05 \mu\text{m}$  and  $1.55 \mu\text{m}$  are shown in Figs. 3(a) and 3(b), respectively. From Fig. 3(a),  
 108 the mode field energies of the  $x$ -pol and  $y$ -pol odd and even modes do not occur to change at  
 109 wavelength  $1.05 \mu\text{m}$ , which indicate that before wavelength  $1.05 \mu\text{m}$ , there are no mode coupling  
 110 between the considered modes and SPP modes. From Fig. 3(b), the mode field energy of the  $x$ -  
 111 pol odd mode does not occur to change, and the mode field energies of the  $x$ -pol even,  $y$ -pol odd,  
 112 and  $y$ -pol even modes occur to transfer. It indicates that the  $x$ -pol even,  $y$ -pol odd, and  $y$ -pol even  
 113 modes occur to couple with the  $x$ -pol first SPP mode,  $y$ -pol first SPP mode, and zero SPP mode,  
 114 respectively, after  $1.55 \mu\text{m}$ . Because the coupling strengths based on the SPR effect for different  
 115 modes are different, the effective refractive index differences between the  $x$ -pol and  $y$ -pol modes  
 116 are increased, and the DC-PCF PBS could be achieved due to the enhanced birefringence.

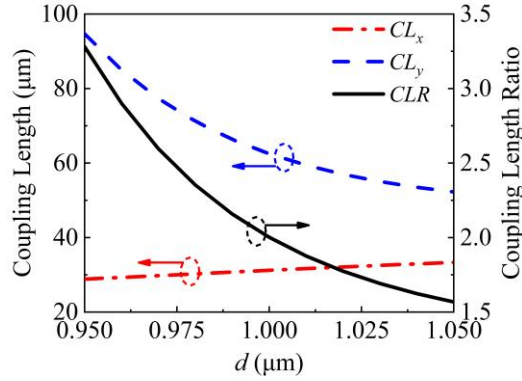


117  
 118 **Fig. 2.** The effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and even modes,  $x$ -pol and  $y$ -pol  
 119 first SPP modes, and zero SPP mode calculated as functions of wavelength.



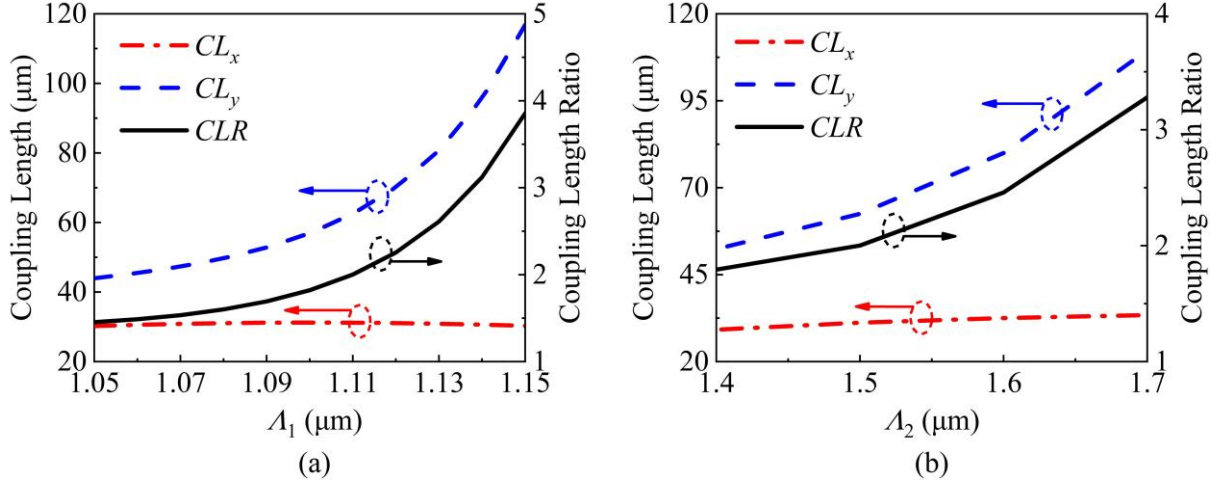
120  
 121 **Fig. 3.** The mode field distributions of the  $x$ -pol odd mode,  $x$ -pol even mode,  $y$ -pol odd mode, and  $y$ -pol even mode  
 122 calculated at wavelengths (a)  $1.05 \mu\text{m}$  and (b)  $1.55 \mu\text{m}$ .

123 In the following, the structure parameters, including  $d$ ,  $A_1$ ,  $A_2$ ,  $d_{x1}$ ,  $d_{y1}$ ,  $d_{y2}$ ,  $d_{x2}$ ,  $d_{x3}$ , and  $d_{y3}$ ,  
 124 are, respectively, adjusted at wavelength 1.55  $\mu\text{m}$  to optimize the performance of the DC-PCF  
 125 PBS. The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$  are shown in Fig. 4. When  $d$   
 126 changes from 0.95 to 1.05  $\mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and even modes  
 127 decrease, but the decrease amplitude of the  $x$ -pol even mode is larger than that of the  $x$ -pol odd  
 128 mode. Meanwhile, the effective refractive indices of the  $y$ -pol odd and even modes also decrease,  
 129 but the decrease amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -pol odd mode. Thus,  
 130 the effective refractive index differences between the  $x$ -pol odd and even modes and  $y$ -pol odd  
 131 and even modes become smaller. As shown in Fig. 4, the  $CL_x$  increases from 28 to 33  $\mu\text{m}$ , and  
 132 the  $CL_y$  decreases from 92 to 52  $\mu\text{m}$ . It can be deduced from Eq. (3) that the  $CLR$  decreases from  
 133 3.2 to 1.5  $\mu\text{m}$ . When  $d=1 \mu\text{m}$ , the  $CLR=2.048$ , which is very close to the ideal value of 2.



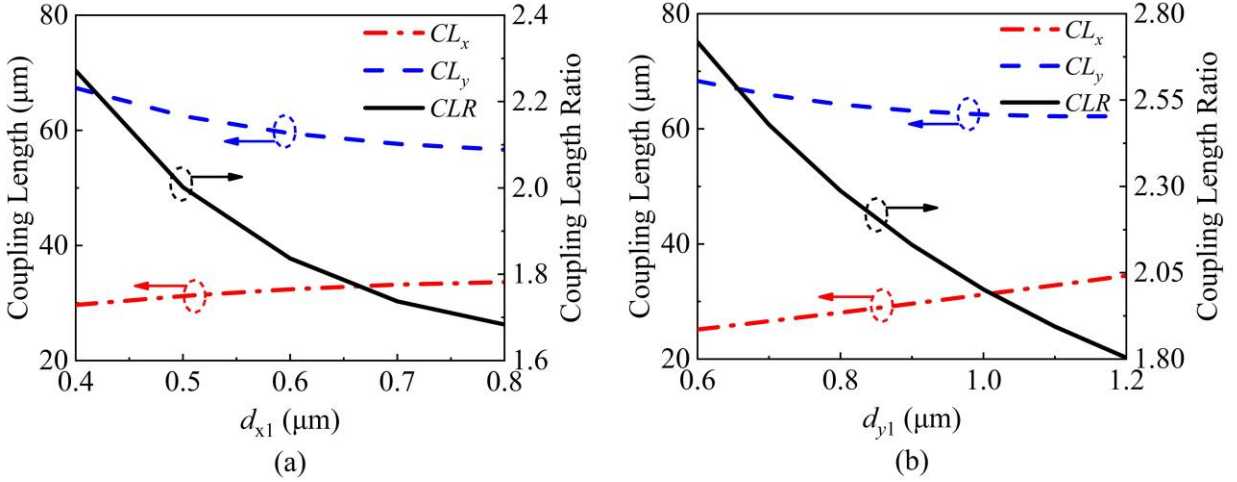
134  
 135 **Fig. 4.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$ .

136 When  $A_1$  changes from 1.05 to 1.15  $\mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and  
 137 even modes increase, and the increase amplitude of the  $x$ -pol even mode is approximately equal  
 138 to that of the  $x$ -pol odd mode. Although the effective refractive indices of the  $y$ -pol odd and even  
 139 modes also increase, the increase amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -  
 140 pol odd mode. Thus, the effective refractive index difference between the  $x$ -pol odd and even  
 141 modes remains almost unchanged, while the effective refractive index difference between the  $y$ -  
 142 pol odd and even modes becomes smaller. As shown in Fig. 5(a), the  $CL_x$  is stabilized at 30  $\mu\text{m}$ ,  
 143 and the  $CL_y$  increases from 43 to 120  $\mu\text{m}$ . According to Eq. (3), the  $CLR$  increases from 1.4 to  
 144 3.8  $\mu\text{m}$ . When  $A_1=1.11 \mu\text{m}$ , the  $CLR$  is very close to 2. From Fig. 5(b), when  $A_2$  changes from 1.4  
 145 to 1.7  $\mu\text{m}$ , the  $CL_x$  increases from 29 to 33  $\mu\text{m}$ , the  $CL_y$  increases from 52 to 109  $\mu\text{m}$ , and the  
 146 corresponding  $CLR$  increases from 1.79 to 3.2. When  $A_2=1.6 \mu\text{m}$ , the  $CLR$  is very close to 2.



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**Fig. 5.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $A_1$  and (b)  $A_2$ .

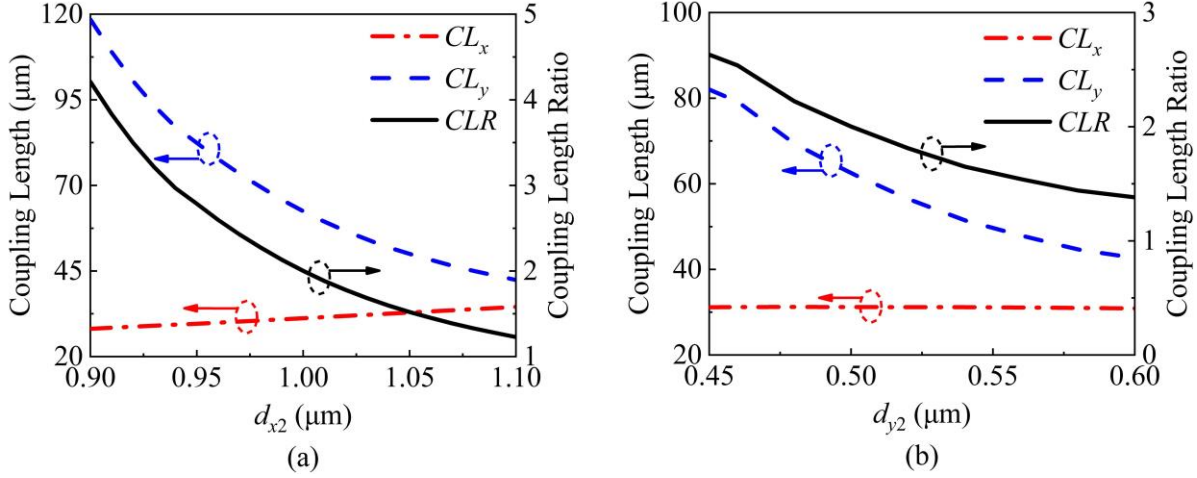


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**Fig. 6.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x1}$  and (b)  $d_{y1}$ .

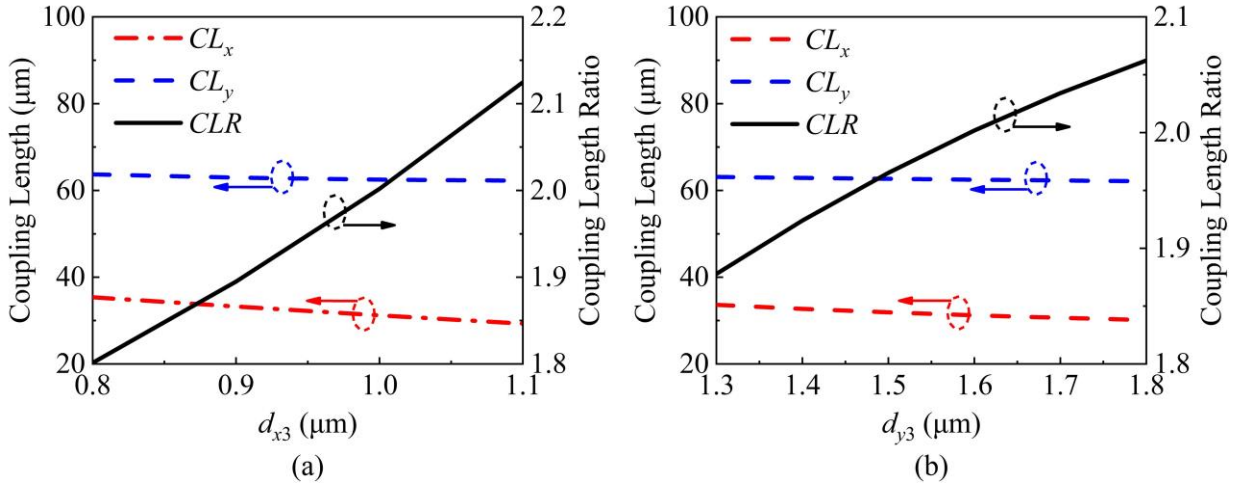
151 The influences of the elliptical hole sizes are shown in Figs. 6(a) and 6(b). When  $d_{x1}$  changes  
 152 from 0.4 to 0.8  $\mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and even modes decrease, but  
 153 the decrease amplitude of the  $x$ -even mode is larger than that of the  $x$ -odd mode. Although the  
 154 effective refractive index of the  $y$ -pol odd mode remains almost unchanged, the effective  
 155 refractive index of the  $y$ -pol even mode gradually decreases. Thus, the effective refractive index  
 156 difference between the  $x$ -pol odd and even modes becomes smaller, and the effective refractive  
 157 index difference between the  $y$ -pol odd and even modes becomes larger. As shown in Fig. 6(a),  
 158 the  $CL_x$  increases from 29 to 33  $\mu\text{m}$ , the  $CL_y$  decreases from 67 to 56  $\mu\text{m}$ , and the corresponding  
 159  $CLR$  decreases from 2.2 to 1.6. When  $d_{x1}=0.5$   $\mu\text{m}$ , the  $CLR$  is very close to 2. When  $d_{y1}$  increases  
 160 from 0.6 to 1.2, the effective refractive index difference of the  $x$ -pol odd and even modes  
 161 becomes smaller, and the effective refractive index difference between the  $y$ -pol odd and even  
 162 modes also becomes larger. As shown in Fig. 6(b), the  $CL_x$  increases from 25 to 34  $\mu\text{m}$ , the  $CL_y$   
 163 decreases from 68 to 62  $\mu\text{m}$ , and the corresponding  $CLR$  decreases from 2.7 to 1.8. When  $d_{y1}=1$   
 164  $\mu\text{m}$ , the  $CLR$  is very close to 2.





165  
166 **Fig. 7.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x2}$  and (b)  $d_{y2}$ .

167 The influences of the elliptical gold wires are shown in Figs. 7(a) and 7(b). When  $d_{x2}$   
168 changes from 0.9 to 1.1 μm, the effective refractive index of the  $x$ -pol odd mode remains almost  
169 unchanged, but the effective refractive index of the  $x$ -pol even mode gradually decreases.  
170 Although the effective refractive indices of the  $y$ -pol odd and  $y$ -pol even modes decrease, the  
171 decrease amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -pol odd mode. Thus, the  
172 effective refractive index difference between the  $x$ -pol odd and  $x$ -pol even modes becomes  
173 smaller, and the effective refractive index difference between the  $y$ -pol odd and  $y$ -pol even  
174 modes becomes larger. As shown in Fig. 7(a), the  $CL_x$  increases from 28 to 34 μm, the  $CL_y$   
175 decreases from 118 to 42 μm, and the corresponding  $CLR$  decreases from 4.2 to 1.2. When  $d_{x2}=1$   
176 μm, the  $CLR=2$ . When  $d_{y2}$  increases from 0.45 to 0.6, the effective refractive index difference  
177 between the  $x$ -pol odd and  $x$ -pol even modes remains almost unchanged, and the effective  
178 refractive index difference between the  $y$ -pol odd and  $y$ -pol even modes becomes larger. As  
179 shown in Fig. 7(b), the  $CL_x$  is stabilized at 30 μm, the  $CL_y$  decreases from 131 to 42 μm, and  
180 the corresponding  $CLR$  decreases from 4.2 to 1.38. When  $d_{y2}=0.5$  μm, the  $CLR$  is very close to 2.

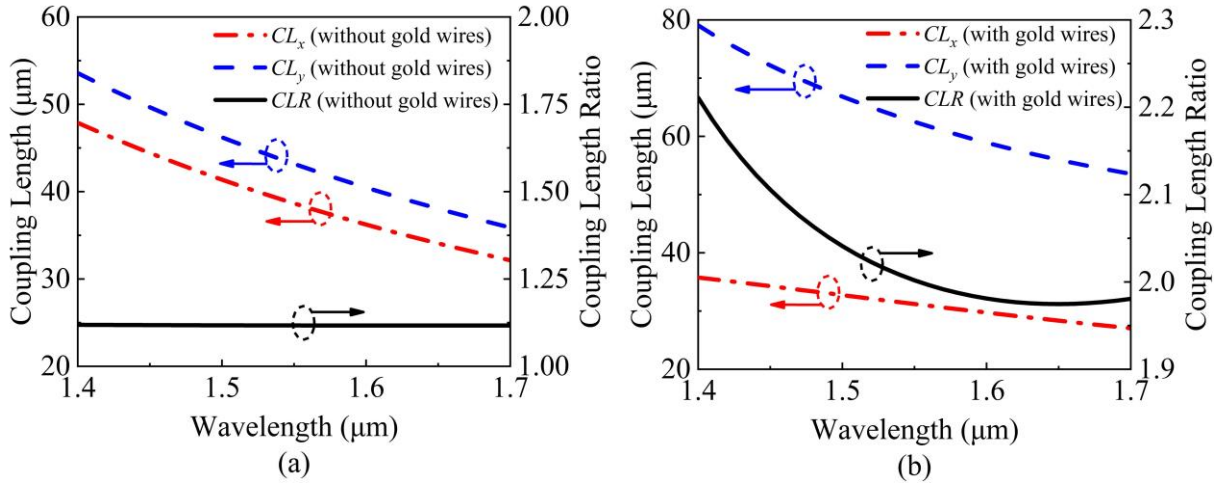


181  
182 **Fig. 8.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x3}$  and (b)  $d_{y3}$ .

183 The influences of the large elliptical air hole along the horizontal axis are shown in Figs. 8(a)  
184 and 8(b). When  $d_{x3}$  changes from 0.8 to 1.1 μm, the effective refractive index of the  $x$ -pol odd

185 mode decreases slightly, and the effective refractive index of the  $x$ -pol even mode remains  
 186 almost unchanged. Meanwhile, the effective refractive indices of the  $y$ -pol odd and  $y$ -pol even  
 187 modes remain almost unchanged. Thus, the effective refractive index difference between the  $x$ -  
 188 pol odd and  $x$ -pol even modes becomes larger, and the effective refractive index differences  
 189 between the  $y$ -pol odd and  $y$ -pol even modes changes slightly. From Fig. 8(a), as the  $CL_x$   
 190 decreases, the  $CL_y$  is almost constant, and the corresponding  $CLR$  increases. As  $d_{y3}$  increases  
 191 from 1.3 to 1.8, the effective refractive indices of the  $x$ -pol odd and  $x$ -pol even modes and  $y$ -pol  
 192 odd and  $y$ -pol even modes decrease, and the decrease amplitudes of the  $x$ -pol odd and  $y$ -pol odd  
 193 modes are approximately equal to those of the  $x$ -pol even and  $y$ -pol even modes. It can be seen  
 194 from Fig. 8(b) that the  $CL_x$  and  $CL_y$  are almost constant, but the corresponding  $CLR$  increases.

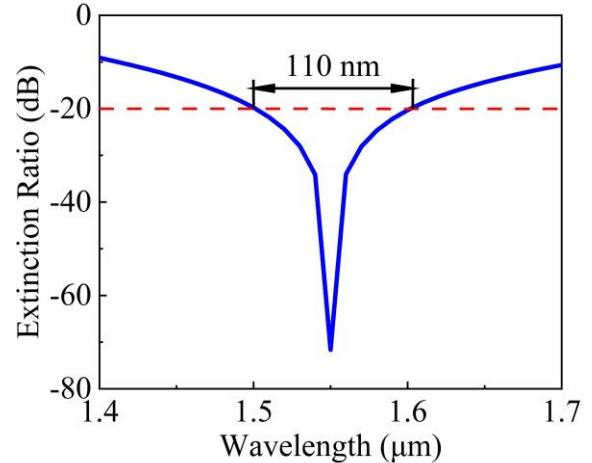
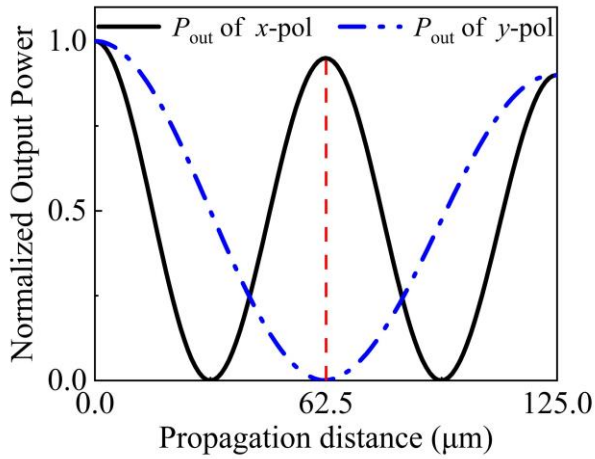
195 As shown in Fig. 9(a), when the gold wire is not filled in the two elliptical air holes, the  
 196  $CLR$  can only maintain at 1.1 in the wavelength range from 1.4 to 1.7  $\mu\text{m}$ . At this time, it is  
 197 difficult to completely split the polarized light between the two cores. As shown in Fig. 9(b),  
 198 when the two elliptical air holes are filled with the gold wires, the  $CLR$  decreases from 2.21 to  
 199 1.98 in the considered wavelength range, and reaches 2 at wavelength 1.55  $\mu\text{m}$ . Therefore, the  
 200 gold wire plays an important role in achieving the PBS.  
 201



202  
 203 **Fig. 9.** The relationships between the  $CL$  and  $CLR$  and wavelength, (a) without gold wires, and (b) with gold wires.

204 In summary, the optimized structure parameters of the DC-PCF PBS are chosen as  
 205 following:  $A_1=1.11 \mu\text{m}$ ,  $A_2=1.5 \mu\text{m}$ ,  $d=1 \mu\text{m}$ ,  $d_{x1}=0.5 \mu\text{m}$ ,  $d_{y1}=1 \mu\text{m}$ ,  $d_{x2}=1 \mu\text{m}$ ,  $d_{y2}=0.5 \mu\text{m}$ ,  $d_{x3}=1$   
 206  $\mu\text{m}$ , and  $d_{y3}=1.6 \mu\text{m}$ . Fig. 10(a) shows the relationship between  $P_{\text{out}}$  of  $x$ -pol and  $y$ -pol and  
 207 propagation distance. As shown in Fig. 10(a), when the light at wavelength 1.55  $\mu\text{m}$  enters the  
 208 core A,  $P_{\text{out}}$  of the  $x$ -pol and  $y$ -pol will periodically change with the propagation distance. When  
 209 the propagation distance is 62.5  $\mu\text{m}$ ,  $P_{\text{out}}$  of the  $x$ -pol reaches the maximum value, and  $P_{\text{out}}$  of the  
 210  $y$ -pol is close to 0. At this time, the two polarization states can be completely separated. For the  
 211 core B, the case is exactly opposite. Due to the ohmic loss of metal, the maximum value of the  
 212 normalized power will decrease with the propagation distance 36. Thus, the optimal DC-PCF  
 213 PBS length is 62.5  $\mu\text{m}$ . Fig. 10(b) shows the relationship between the  $ER$  and wavelength when  
 214 the DC-PCF PBS length is 62.5  $\mu\text{m}$ . It can be seen from Fig. 10(b) that the  $ER$  reaches the  
 215 maximum value of -71 dB at wavelength 1.55  $\mu\text{m}$ , and is less than -20 dB in the wavelength  
 216 range of 1.5 to 1.61  $\mu\text{m}$ . The bandwidth of the DC-PCF PBS is 110 nm, covering the whole C  
 217 band.





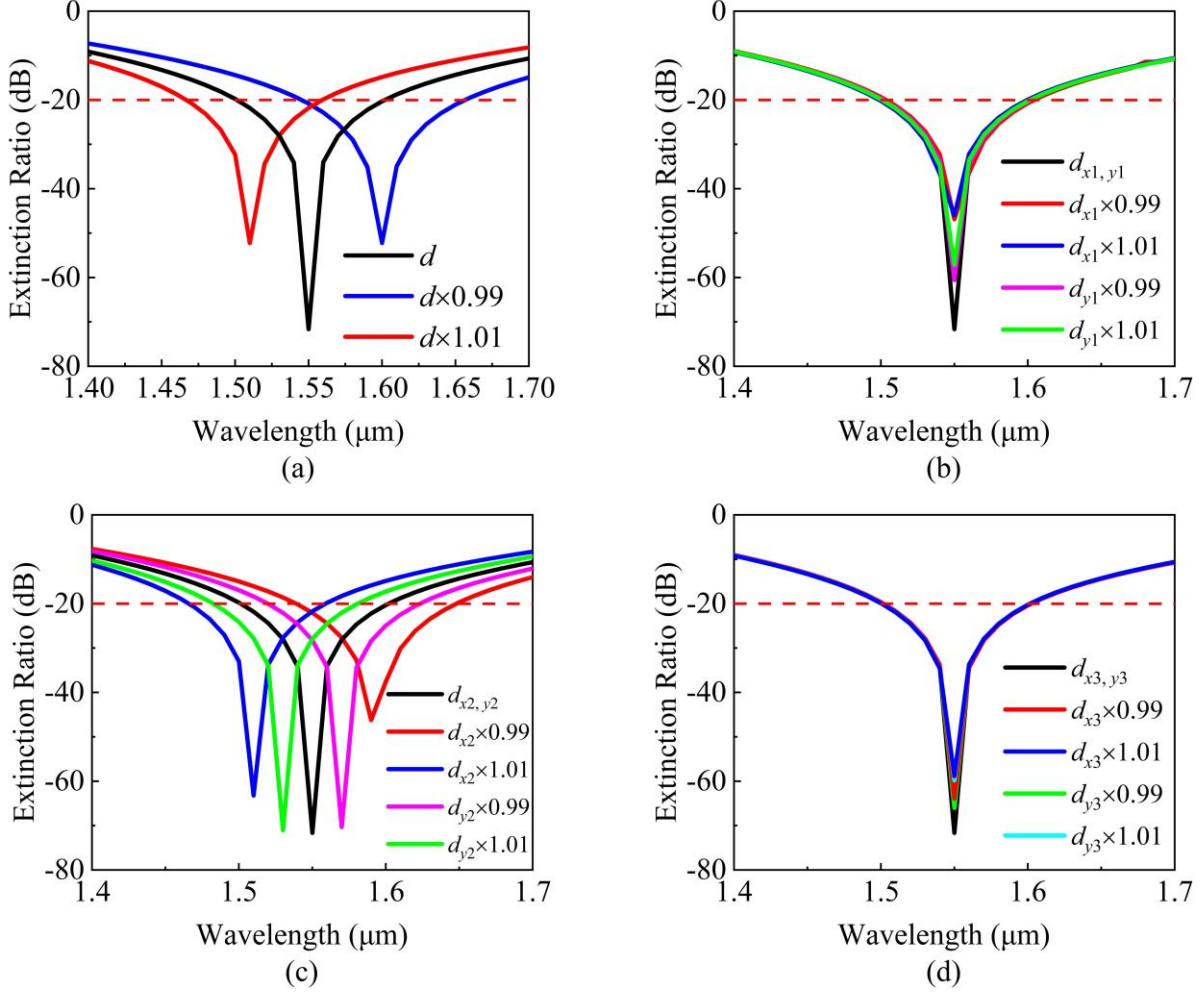
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**Fig. 10.** (a) The relationship between  $P_{out}$  of the  $x$ -pol and  $y$ -pol and propagation distance, and (b) the relationship between the  $ER$  and wavelength.

221

Table 1. The comparisons between other proposed PCF PBSs and this work.

Reference	PBS length	Bandwidth	$ER$ at 1550 nm
22	1.890 mm	9 nm	-83.2 dB
23	0.175 mm	250 nm	-80.7 dB
25	1.0 mm	280 nm	-83.6 dB
26	1.746 mm	47 nm	-60 dB
<b>Error! Reference source not found.</b>	830 $\mu$ m	20 nm	-60 dB
[42]	254.6 $\mu$ m	560 nm	-111 dB
This work	62.5 $\mu$ m	110 nm	-71 dB



**Fig. 11.** The relationships between the *ER* and wavelength under  $\pm 1\%$  error of (a)  $d$ , (b)  $d_{x1}$ ,  $d_{y1}$  (c)  $d_{x2}$ ,  $d_{y2}$ , and (d)  $d_{x3}$ ,  $d_{y3}$ .

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Table 1 shows the comparisons between other proposed PCF PBSs and this work [37-42]. It can be concluded from Table 1 that although the bandwidths of the PBSs proposed in Refs [38, 39, 42] are slightly wider than that of this work, the DC-PCF PBS proposed in this work has the shortest length. This is more conducive to the development of photonic integration. Moreover, the bandwidth and *ER* are also good. Finally, we will consider the fabrication tolerance of the proposed DC-PCF PBS. We investigated the dependence of the *ER* on each structure parameter under the fabrication tolerance of 1%. As shown in Fig. 11(a), when  $d$  is reduced or increased by 1%, the bandwidth is red-shifted to 1.54 - 1.64  $\mu\text{m}$  or blue-shifted to 1.46 - 1.56  $\mu\text{m}$ . The DC-PCF PBS can still work well. As shown in Figs. 11(b) and 11(d), when  $d_{x1}$  and  $d_{y1}$ , and  $d_{x3}$  and  $d_{y3}$  are reduced or increased by 1%, only the *ER* at wavelength 1.55  $\mu\text{m}$  is changed, and the bandwidth of the proposed DC-PCF PBS does not change. As shown in Fig. 11(c). when  $d_{x2}$  and  $d_{y2}$  are reduced by 1%, the bandwidth is blue-shifted to 1.53 - 1.65  $\mu\text{m}$  and 1.51 - 1.63  $\mu\text{m}$ , respectively. When  $d_{x2}$  and  $d_{y2}$  are increased by 1%, the bandwidth is red-shifted to 1.43- 1.57  $\mu\text{m}$  and 1.41- 1.57  $\mu\text{m}$ , respectively. Therefore, the proposed DC-PCF PBS has good fabrication tolerance.

#### 240 4. Conclusion

241 In conclusion, we design an ultra-short DC-PCF PBS based on the SPR effect. The performance  
242 of the proposed DC-PCF PBS is optimized through adjusting structure parameters. The *CLR* at  
243 wavelength 1.55  $\mu\text{m}$  is very close to 2. The optimized DC-PCF PBS length is 62.5  $\mu\text{m}$ , the *ER* at  
244 wavelength 1.55  $\mu\text{m}$  is -68.76 dB, and the bandwidth is 110 nm (1.5 - 1.61  $\mu\text{m}$ ), which can cover  
245 the whole C band. The proposed DC-PCF PBS has ultra-short length, large bandwidth, and high  
246 *ER*, and can find important application in the micro-optical system.

#### 247 Disclosures

248 The authors declare no conflicts of interest.

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#### 391 **Captions List**

392 **Fig. 1.** The cross-section of the proposed DC-PCF PBS.

393 **Fig. 2.** The effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and even  
394 modes,  $x$ -pol and  $y$ -pol first SPP modes, and zero SPP mode calculated as functions of  
395 wavelength.

396 **Fig. 3.** The mode field distributions of the  $x$ -pol odd mode,  $x$ -pol even mode,  $y$ -pol odd mode,  
397 and  $y$ -pol even mode calculated at wavelengths (a) 1.05  $\mu\text{m}$  and (b) 1.55  $\mu\text{m}$ .

398 **Fig. 4.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$ .

399 **Fig. 5.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $A_1$  and (b)  $A_2$ .

400 **Fig. 6.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x1}$  and (b)  $d_{y1}$ .

401 **Fig. 7.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x2}$  and (b)  $d_{y2}$ .

402 **Fig. 8.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x3}$  and (b)  $d_{y3}$ .

403 **Fig. 9.** The relationships between the  $CL$  and  $CLR$  and wavelength, (a) without gold wires, and  
404 (b) with gold wires.

405 **Fig. 10.** The relationship between  $P_{\text{out}}$  of the  $x$ -pol and  $y$ -pol and propagation distance, and (b)  
406 the relationship between the  $ER$  and wavelength.

407 **Fig. 11.** The relationships between the  $ER$  and wavelength under  $\pm 1\%$  error of (a)  $d$ , (b)  $dx_1$ ,  $dy_1$   
408 (c)  $dx_2$ ,  $dy_2$ , and (d)  $dx_3$ ,  $dy_3$ .

409 **Table 1.** The comparisons between other proposed PCF PBS and this work.